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A STUDY OF THE IMPULSE VALVE
FOR UGANDA HYDRAULIC RAM PUMP

BY

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Background

E. Schiller and P. Kahangire carried out an experimental (1) and an analytical study (2) of the automatic hydraulic ram pump. In the analytical study, the impulse valve was assumed to close instantaneously. This restrictive assumption was necessitated by the lack of knowledge of the dynamic behaviour of the impulse valve at the time. The present study seeks to develop a mathematical model for predicting the dynamic behaviour of the impulse valve as it closes. Such a model will lead us to a better understanding of how the shape of the impulse valve affect the performance of the hydraulic ram. This will enable us to improve the design of the impulse valve for optimum performance of the hydraulic ram.

The Mathematical Model

The accompanying paper (3) describes a mathematical model for an impulse valve with a weighted valve flap. In the mathematical model, the one-dimensional fluid flow equations of the hydram cycle are solved by a numerical finite difference method. The finite difference method is chosen because quite complex physical models can be incorporated into the solution procedure via the finite difference formulation. The computer program contains about 550 lines of FORTRAN statements and it takes about 2.5 minutes to compute a complete hydram cycle (2500 iterations) on an IBM-XT compatible.

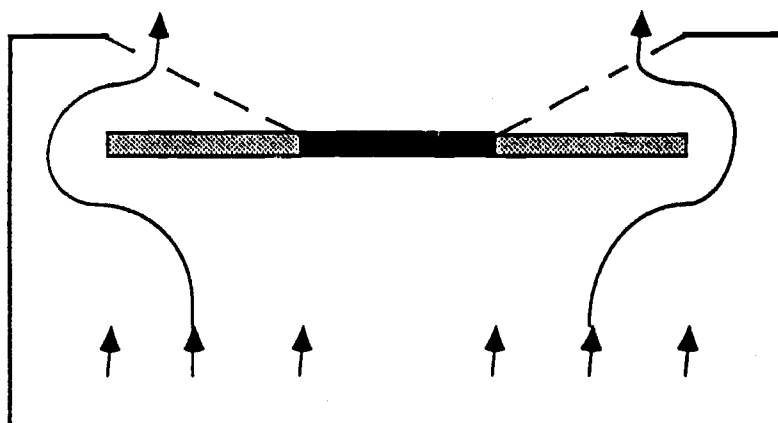


Fig. 1: Schematic diagram of the impulse valve

In the present study, the valve arrangement is different. The valve flap is a rubber disc with a central location hole. The central hole fits into a vertical sleeve which positions it to close upwards onto a perforated (the orifice) conical valve seat (see Fig. 1). As the water flows upwards past the outer edges of the valve flap and into the orifice, a pressure difference is generated between the bottom and top surfaces of the valve flap. As the pressure on the bottom surface is higher, the outer edge of the valve flap is pushed upwards. If the flow is fast enough, the valve flap closes itself on to the conical valve seat and stops the flow. The mathematical model as described in reference 3 still applies except that there is no period 2. In period 3, the movement of the outer edge of the valve flap is computed from an algebraic expression which gives the relationship between the deflection of the outer edge and the pressure difference between the top and bottom surfaces of the valve flap.

Experimental Investigation

A parallel experimental investigation was carried out to obtain data to test the numerical computational prediction procedure. Experiments were run for different rubber hardness as well as different thickness.

Physical Models

Deflection of Rubber Flap

The rubber valve flap is assumed to deflect under a uniform pressure loading p . The deflection of the outer edge of the rubber flap is given by:

$$y_{\max} = \frac{3 p a^4 (1-\nu^2)}{16 E h^3} \left[\frac{4 (1-s^2) (3+\nu)}{(1+\nu)} + \frac{16 s^2 (1+\nu) (\ln(1/s))^2}{(1-\nu) (1-s^2)} - \frac{4 s^2 (3+\nu) \ln(1/s)}{(1-\nu)} - \frac{(1-s^4) (5+\nu)}{(1+\nu)} \right]$$

where

y_{\max} is the deflection at the outer edge
 a is the outer radius of rubber disc
 b is the inner radius of rubber disc
 s is the ratio (b/a)
 ν is the Poisson's ratio of rubber

The effective pressure exerting on the rubber disc is computed from the expression

$$p = 0.5 \rho V_a^2 (C_d + C_a) + 0.5 V_r^2 C_r$$

where

V_a is the velocity at the tip of the valve flap
 V_r is the radial velocity between the valve flap and valve seat
 C_d, C_a, C_r are pressure loss coefficients

The Computer Program

A listing of the computer program is attached. An explanation of the meaning of the variables are given at the beginning of the program.

Results and Discussion

Although the present prediction procedure employs a simple quasi-steady model for the closure of the impulse valve flap, it is possible to procure agreement with the experimental results of the rate of closure of the valve flap (see Fig. 2 to 7) by suitable adjustment of the pressure coefficient C .

The theoretical predictions of global performance data (such as volumetric flow rates through the impulse and the delivery valves, and the number of beats per minute) are compared with the experimental results in Tables 1 and 2. The trend shown by the experimental results are well predicted by the present model. However, the predicted water flowrates through both the impulse and delivery valves fall at a slower rate than the experimental values.

References

1. Schiller, E.J., Kahangire, P. (1984) "An experimental investigation and design of hydraulic ram pumps". International Journal for Development Technology, Vol. 2, 173 - 183.
2. Schiller, E.J., Kahangire, P. (1984) "Analysis and computerised model of the automatic hydraulic ram pump". CAN. J. CIV. ENG. Vol. 11.
3. Goh, S.Y. (1988) "A study of the dynamic characteristics of the impulse valve of the hydraulic ram". Paper presented at the 6th IWRA World Congress on Water Resources, May 29 - June 3, 1988, Ottawa, Canada.

TABLE 1

	<u>Expt.</u>	<u>Theory</u>	<u>Expt.</u>	<u>Theory</u>	<u>Expt.</u>	<u>Theory</u>
Elasticity	540000	540000	540000	540000	540000	540000
Thickness	.00635	.00635	.00953	.00953	0.0127	0.0127
Delivery Pressure (psig)		60	54	60		60
Q (litres/min)		19.3	21.2	40.6		72
q (litres/min)		0.548	0	1.45		2.33
Beats (per min)		138.5	51	85.5		57
Delivery Pressure		50	50	50	52	50
Q (litres/min)		19.9	23.7	41.1	34.5	72.8
q (litres/min)		0.79	0.16	1.83	0.28	2.87
Beats (per min)		142.3	52	86.6	49	57.6
Delivery Pressure		40	37	40	37	40
Q (litres/min)		20.1	31.6	41.6	43	73.6
q (litres/min)		1.11	0.98	2.38	1.46	3.68
Beats (per min)		144.4	58	87.7	51	58.2
Delivery Pressure	28	30	30	30	30	30
Q (litres/min)	8.4	19.3	33.7	41.5	48.1	74.5
q (litres/min)	0	1.53	1.58	3.24	2.52	5.01
Beats (per min)	89	138.4	58	87.5	51	58.9
Delivery Pressure	21	20	17	20	17	20
Q (litres/min)	14.5	17.9	43.3	42.8	59.1	75.4
q (litres/min)	1.08	2.25	4.8	5.09	6.36	7.66
Beats (per min)	102	128.6	62	90.3	57	59.6
Delivery Pressure	10	10	12	10		10
Q (litres/min)	18.4	19	44.2	43.6		74.9
q (litres/min)	4.32	4.91	8.61	10.5		15.3
Beats (per min)	100	136.4	63	92.1		59.2

TABLE 2

	<u>Expt.</u>	<u>Theory</u>	<u>Expt.</u>	<u>Theory</u>
Elasticity	1510000	1510000	1510000	1510000
Thickness	0.00635	0.00635	0.00953	0.00953
Delivery Pressure (psig)		60	58	60
Q (litres/min)		36.3	40.9	80.8
q (litres/min)		1.29	0.16	2.48
Beats (per min)		93.7	42	51.3
Delivery Pressure		50	50	50
Q (litres/min)		36.7	45.2	82.3
q (litres/min)		1.64	0.54	3.07
Beats (per min)		94.7	43	52.3
Delivery Pressure	41	40	41	40
Q (litres/min)	16	36.5	49.1	83.1
q (litres/min)	0.245	2.11	0.78	3.92
Beats (per min)	68	94.4	44	52.8
Delivery Pressure	30	30	29	30
Q (litres/min)	24	37.1	55.5	84
q (litres/min)	1.25	2.93	1.88	5.33
Beats (per min)	74	95.7	45	53.3
Delivery Pressure	20	20	23	20
Q (litres/min)	23.2	37.7	62.1	84.9
q (litres/min)	1.98	4.56	2.94	8.13
Beats (per min)	73	97.3	46	53.9
Delivery Pressure	11	10	10	10
Q (litres/min)	25.9	38.5	81.3	83.6
q (litres/min)	5.64	9.42	10.9	16.1
Beats (per min)	71	99.5	52	53.1

FIG. 2a & 2b : VARIATION OF PRESSURE & IMPULSE VALVE
DISPLACEMENT DURING CLOSURE.

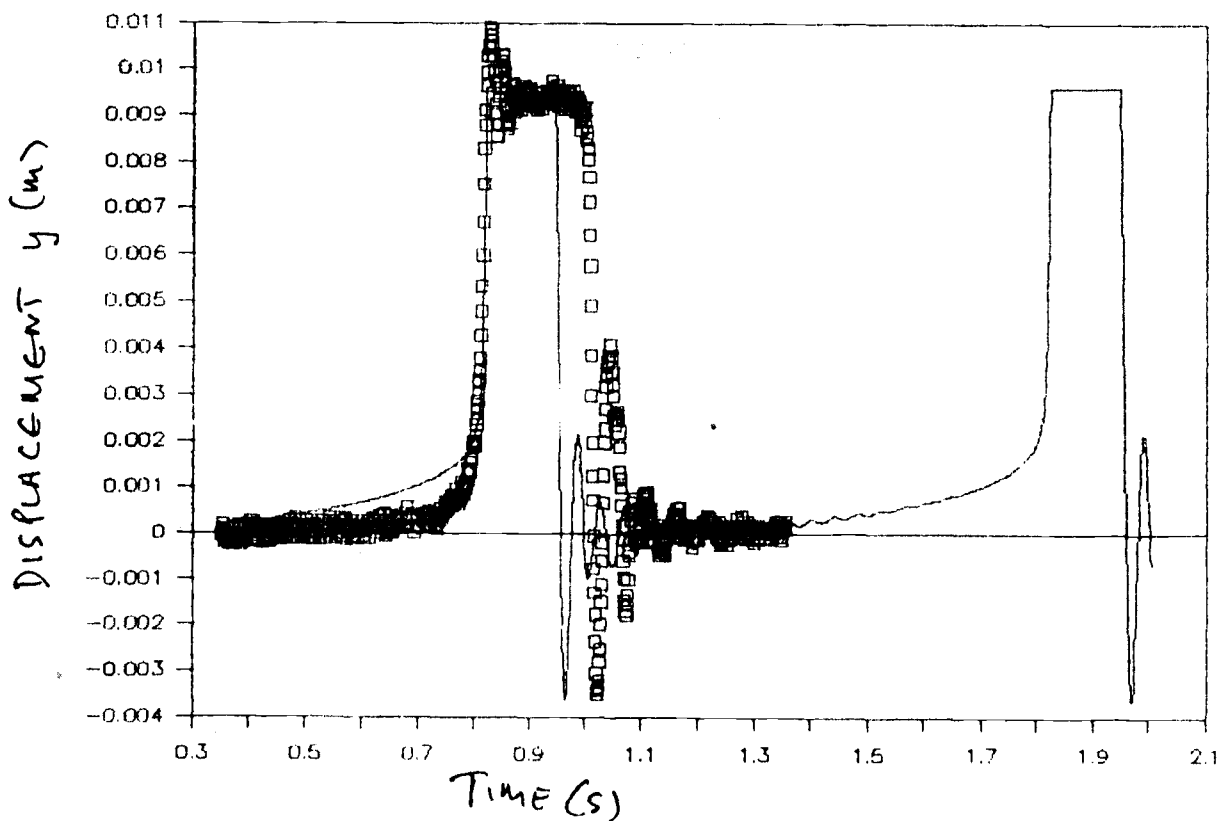
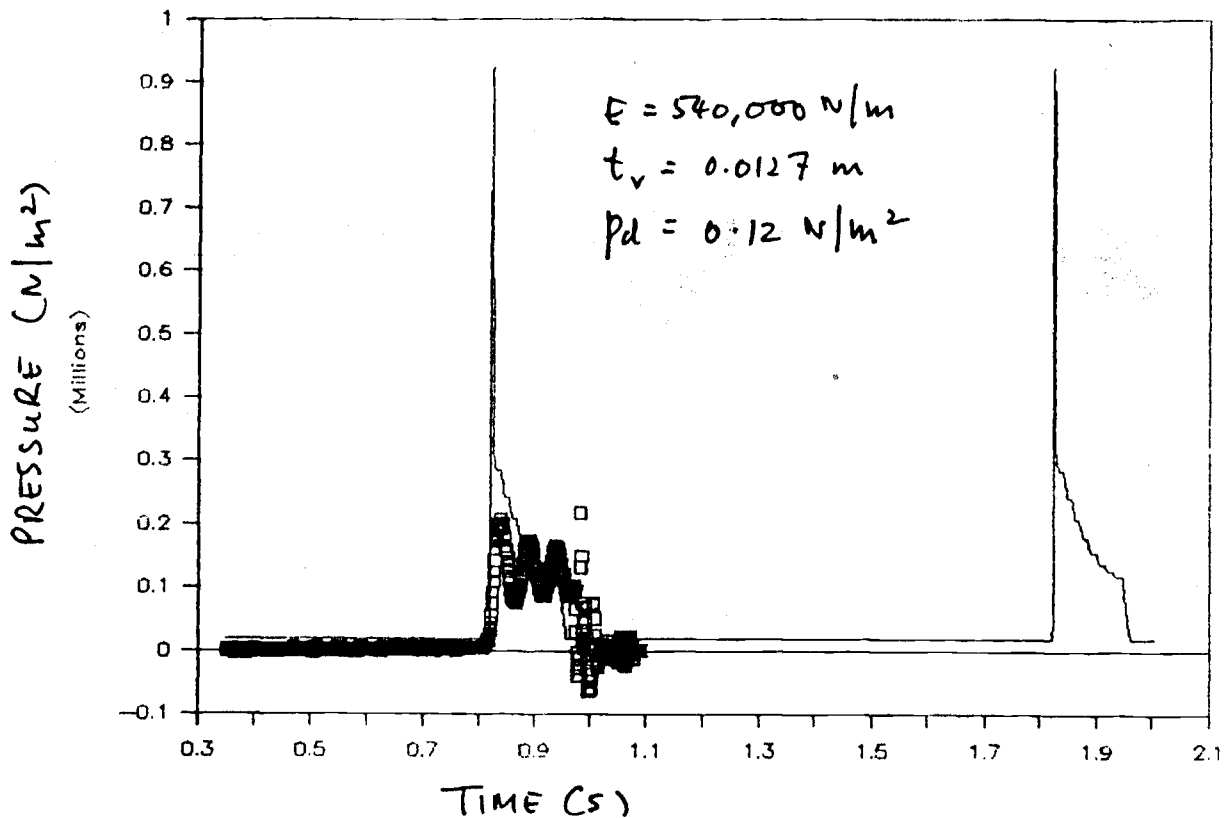


FIG. 3a & 3b : VARIATION OF PRESSURE & IMPULSE VALVE
DISPLACEMENT DURING CLOSURE

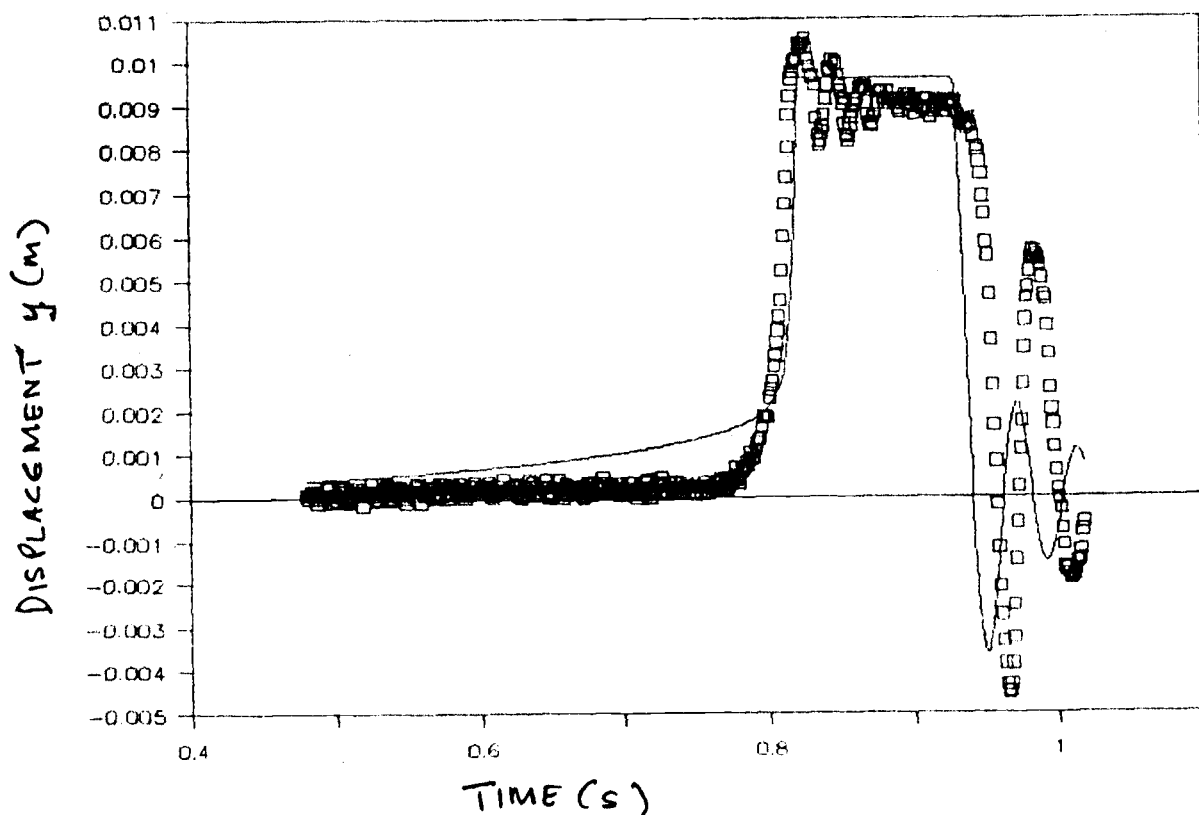
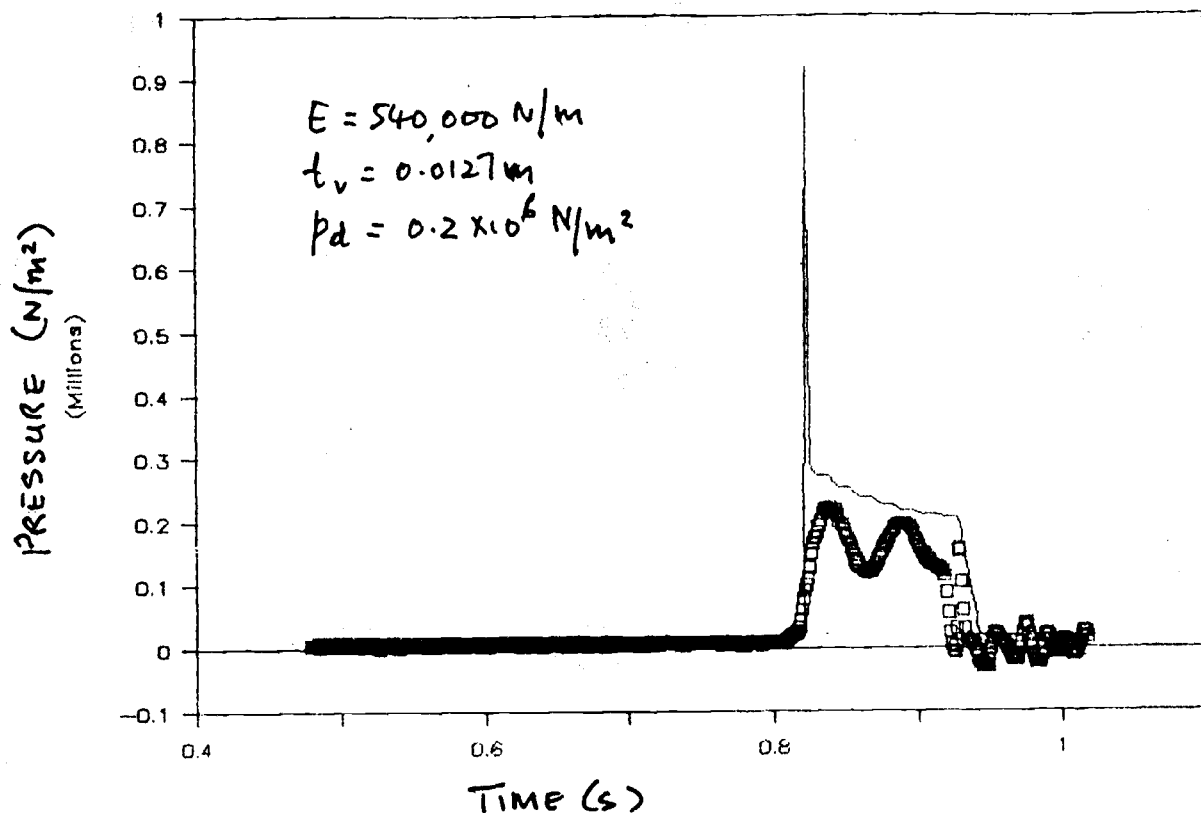


FIG. 4a & 4b

~~FIG. 3a & 3b~~: VARIATION OF VALVE DISPLACEMENT & PRESSURE DURING VALVE CLOSURE

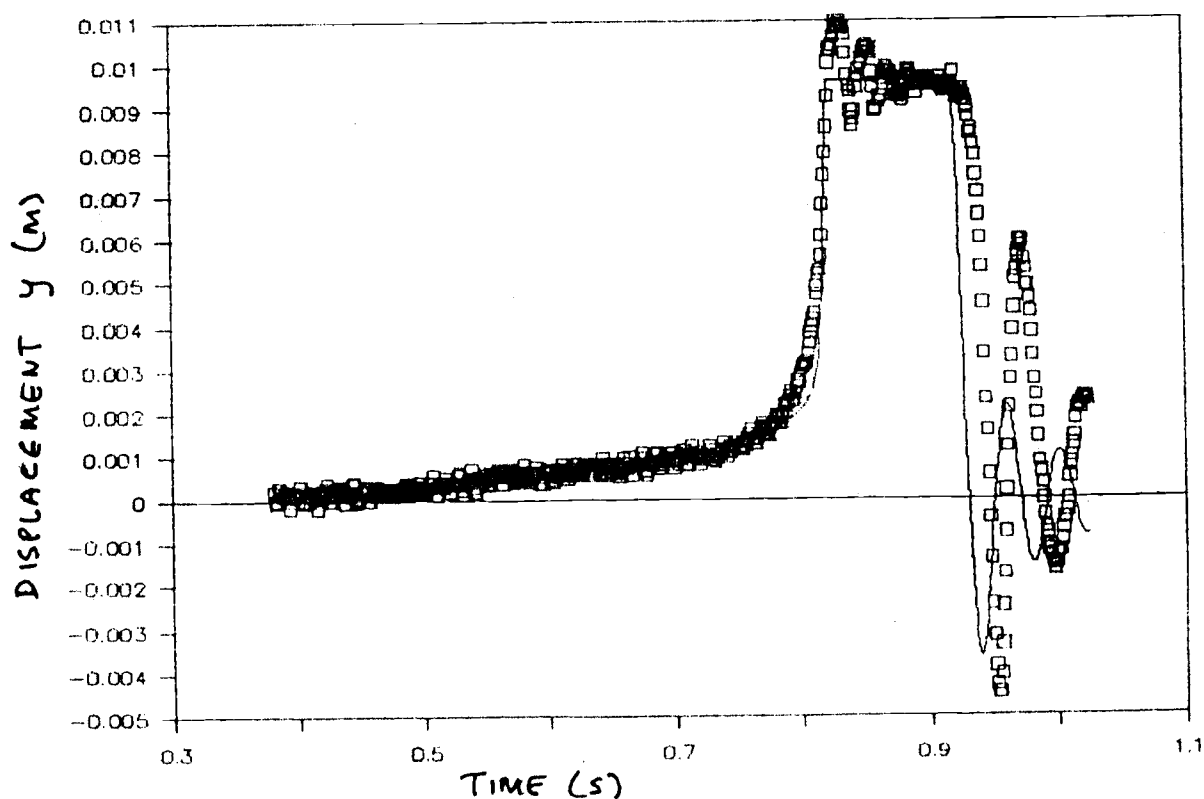
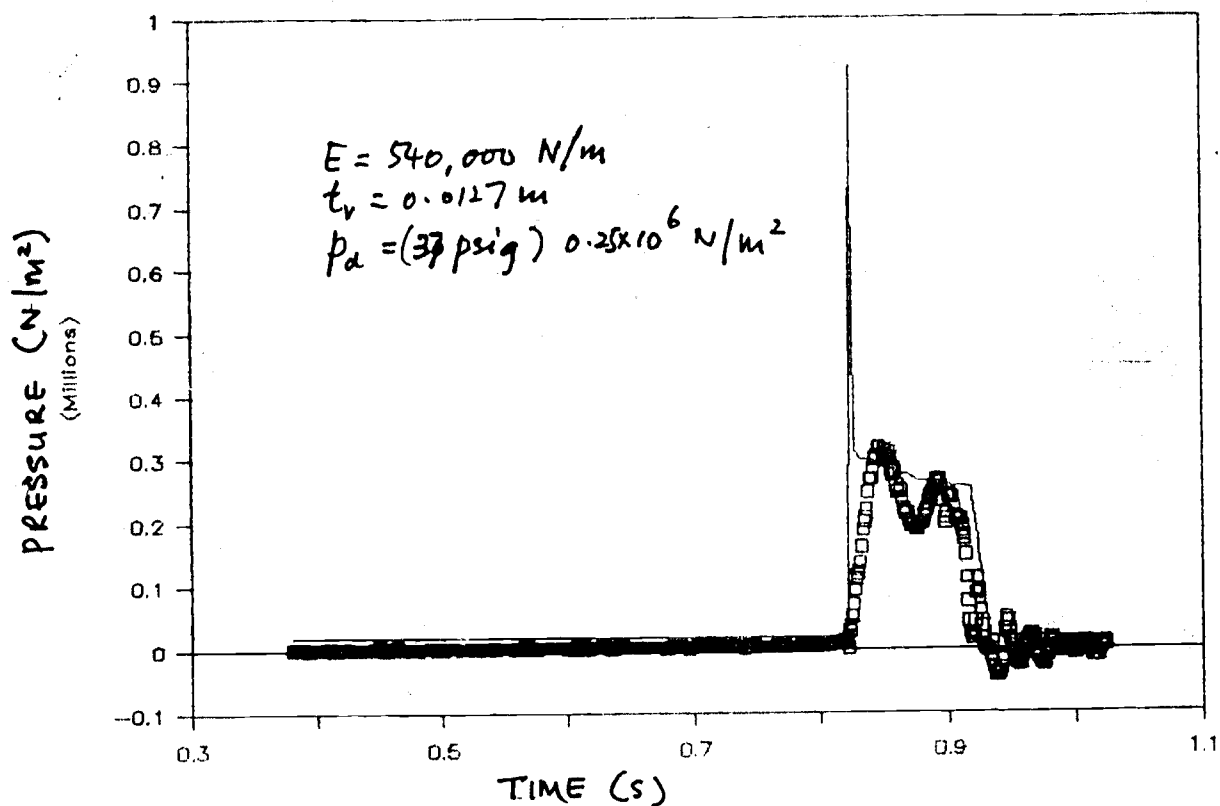


FIG. 5a & 5b : VARIATION OF PRESSURE & IMPULSE VALVE
DISPLACEMENT DURING CLOSURE

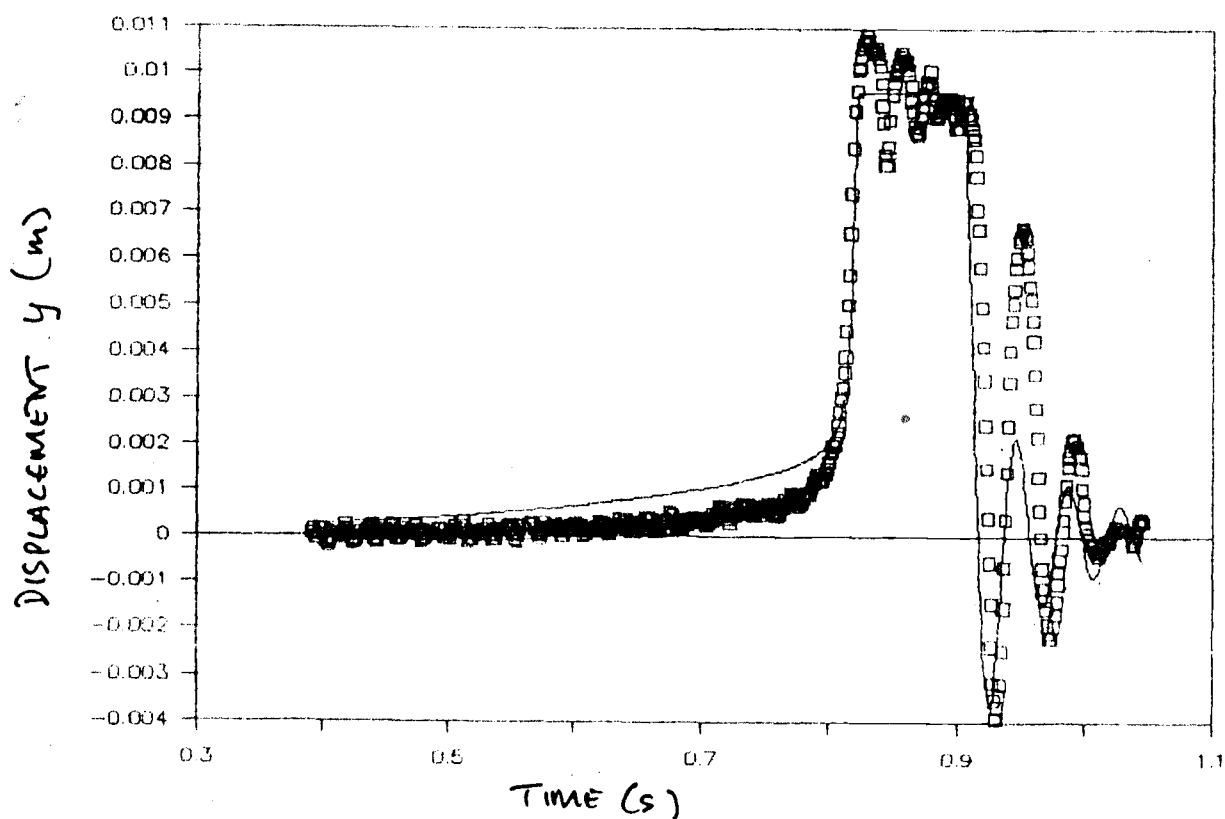
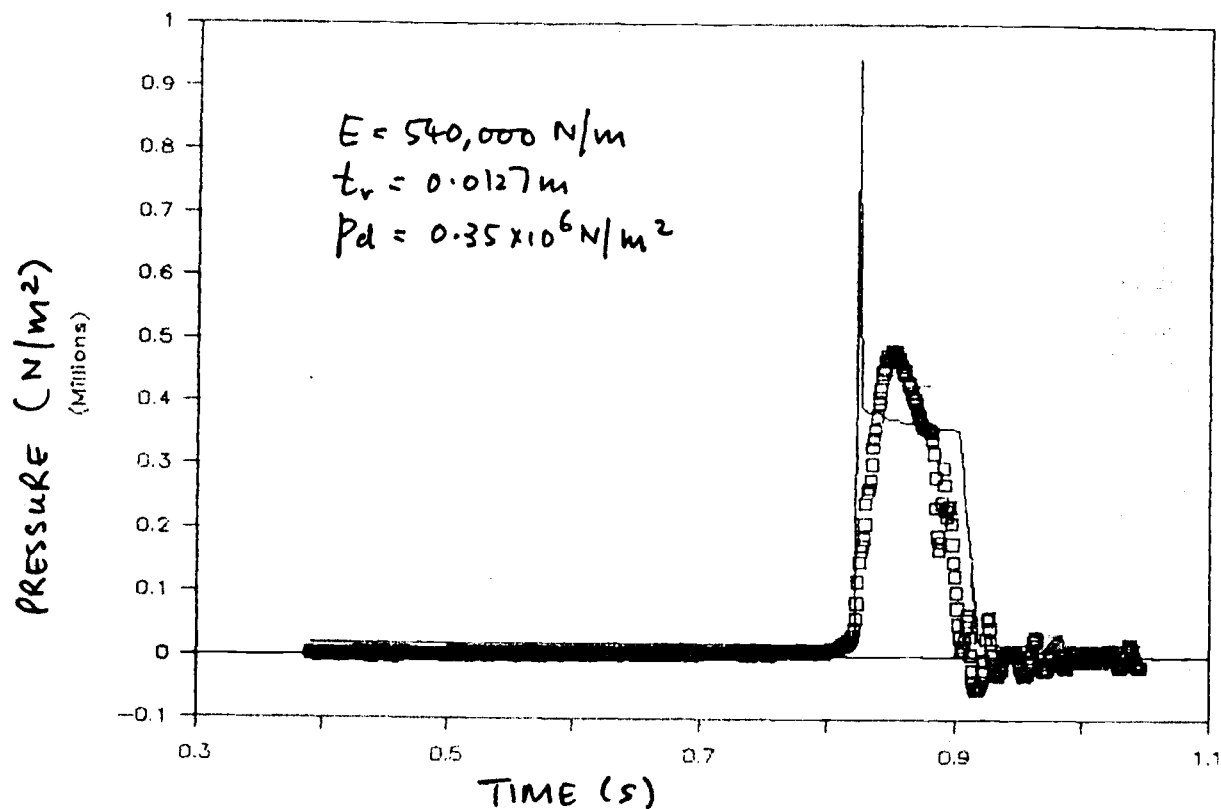


FIG. 6a & 6b: VARIATION OF PRESSURE & IMPULSE VALUE
DISPLACEMENT DURING CLOSURE

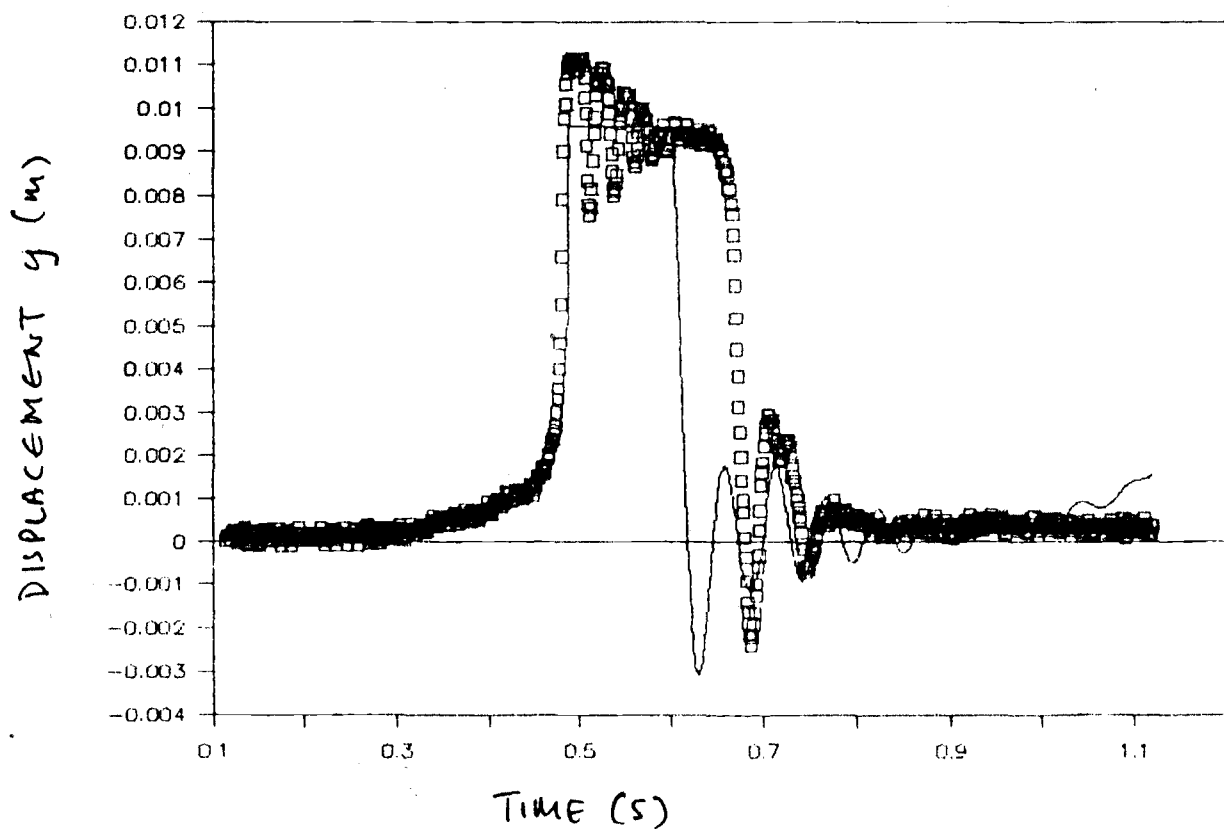
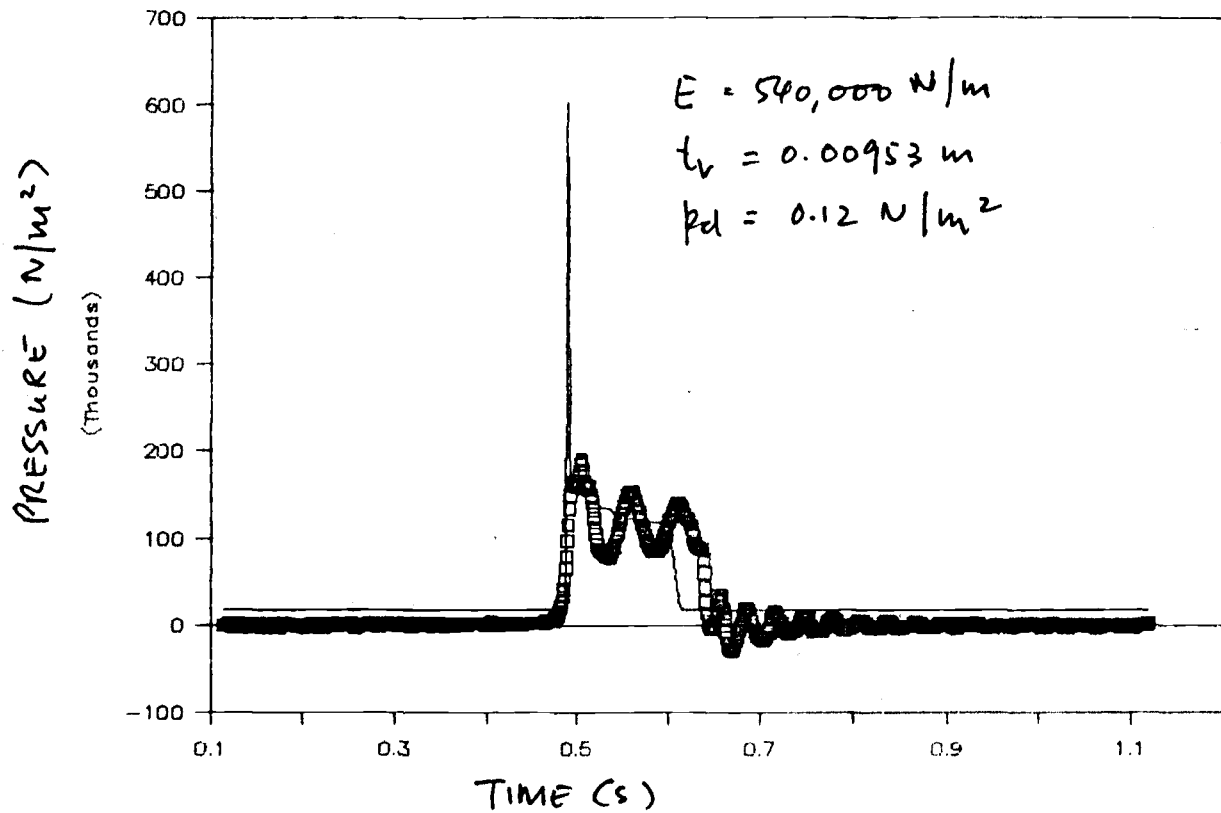
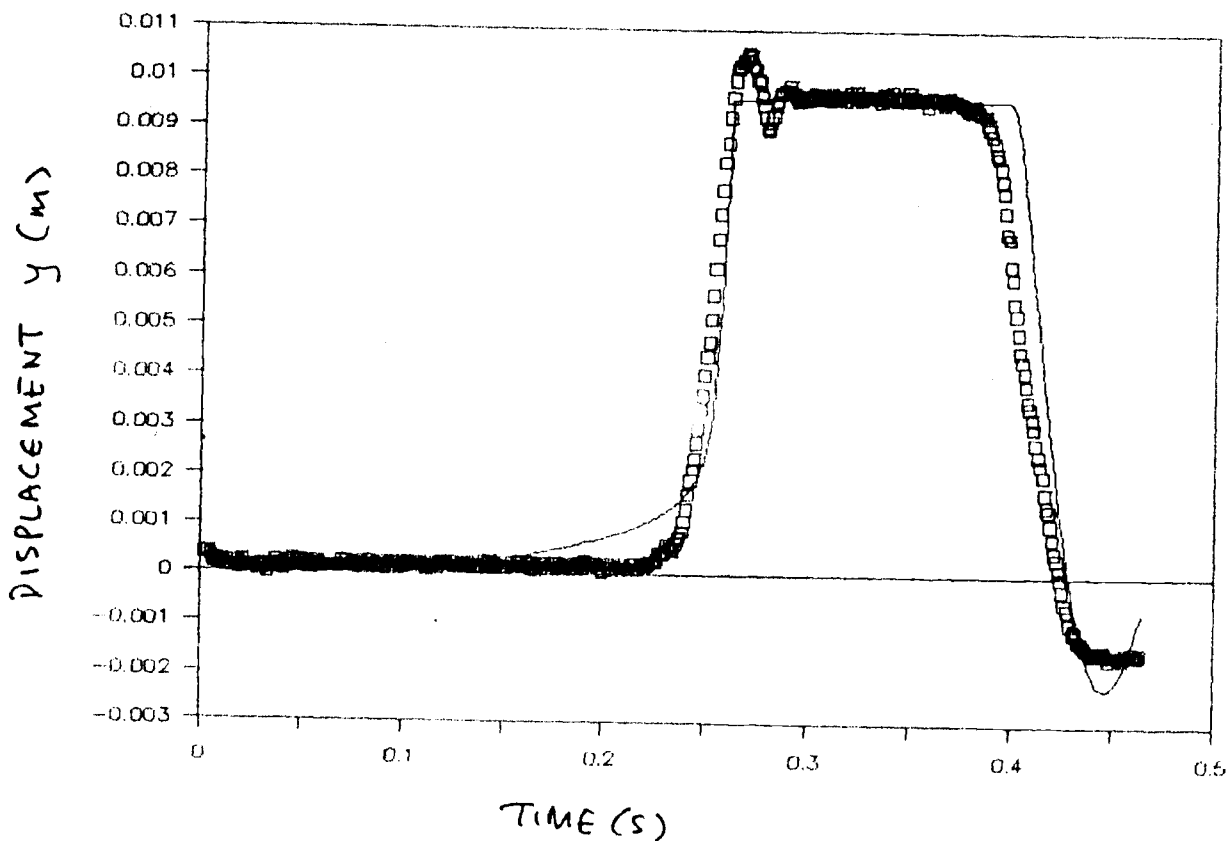
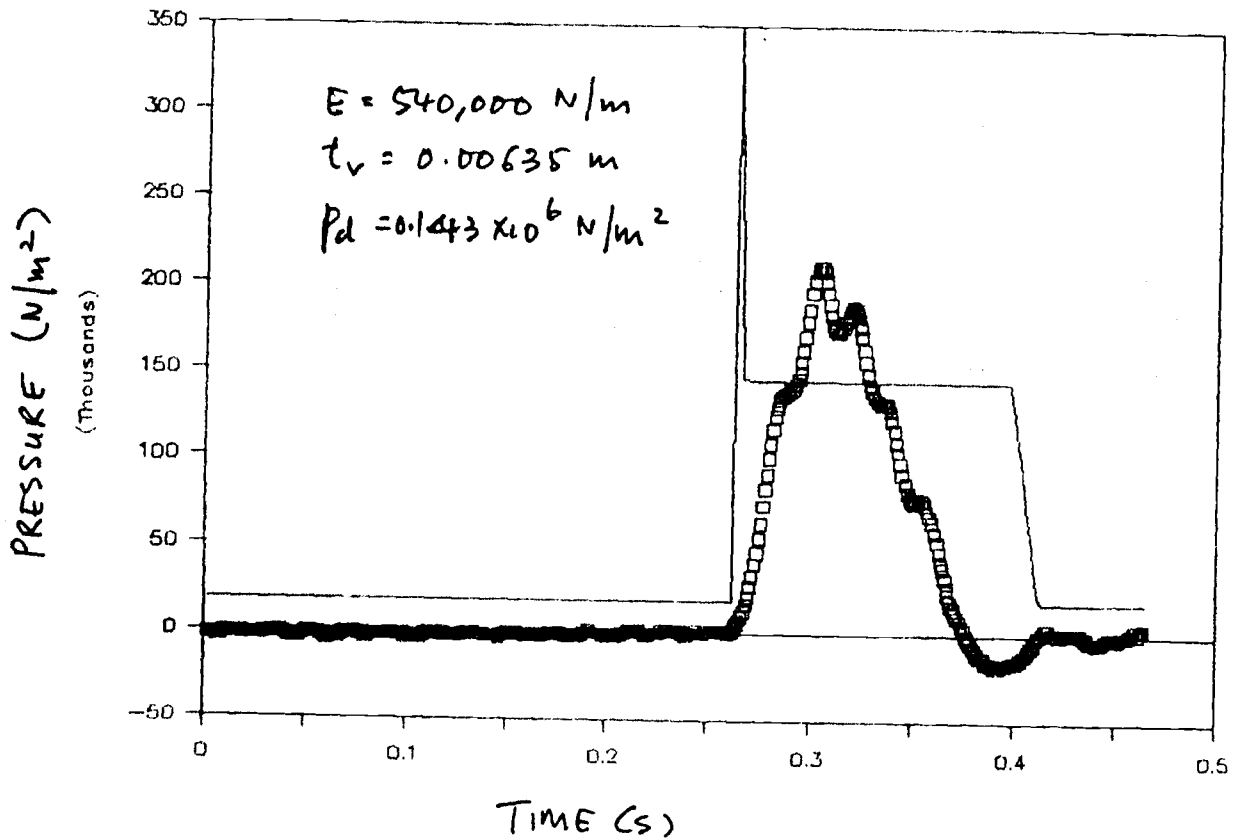


FIG. 7a & 7b : VARIATION OF PRESSURE & IMPULSE VALVE
DISPLACEMENT DURING CLOSURE



PROGRAM FOR PREDICTING THE PERFORMANCE OF A HYDRAULIC RAM PUMP

VERSION 2.0 (26TH MAY 1988) (FORTRAN-77)

WASTE VALVE TYPE: RUBBER DISC FLAP CLOSING UPWARDS ONTO
CONICAL MULTI-HOLE VALVE SEAT

For theoretical background, please refer to:-

' A study of the dynamic characteristics of the
impulse valve of the hydram ' by S.Y. Goh
Paper presented at the 6th IWRA World Conference on Water
Resources, Ottawa, Canada, May 29 - June 3, 1988.

Put ncycle=2 to compute over 2 cycles
nwrite=0 if you do not want a printout of ti,yi,vi etc.
----- drive pipe -----
h is the water drive head
dp is the internal diameter of drive pipe
al is the length of drive pipe
tp is the wall thickness of drive pipe
----- impulse valve -----
a is the external radius of rubber valve flap
b is the internal radius of rubber valve flap
tv is the thickness of the rubber valve flap
er is the Modulus of Elasticity of the rubber
poisr is the Poisson's ratio of the rubber
cdamp is the damping coefficient of valve flap vibration
wn is the frequency of valve flap vibration
freq is factor in frequency formula for valve flap vibration
dor is the effective (single hole) orifice diameter
do is the actual hole diameter of each single hole
alo is the length of the orifice holes
de is the impulse valve chamber diameter
gapmax is the maximum reference gap at outer edge
ymax is the gap when flap is undistorted (flat)
----- delivery valve -----
ddv is the effective (single hole) delivery valve diameter
----- properties -----
den is the density of water
vis is the viscosity of water
ew is the Bulk Modulus of water
es is the Modulus of Elasticity of steel
pois is the Poisson's ratio for steel
----- output -----
qwlpm is the flowrate through the impulse valve (litres per min)
qtlpm is the flowrate through the delivery valve (litres per min)
beat is the number of beats (cycles) per minute

The results will be stored in a file 'RESULT'.
This file can be printed out or examined through an editing
program.

common/gen/ctp,cte,ctda,ctr,ap,arpo,arop,vpi,vpim1
1 ,voi,vpmax,qwaste,pr,dt,pstat
common/dimen/h,dp,tp,al,alo,do,dor,de,ddv
common/prop/den,vis,ew,es,pois
common/press/pa,papsi,pdgpsi
common/coeff/cp,cdv,cd,ca,cr1,cr2,co
common/flap/a,b,tv,er,poisr,cdamp,freq

```

c -----
c      open(3,file='result')
c .... iteration control parameters .....
c      data ncycle,nmax,nitn,nwrite/2,10000,10,1/
c
c .... specify time step for each period
c      data dt1,dt2,dt3,dt4,dt5,dt6/
c      1      .001,.0005,.0005,.00005,.0005,.0005,.0005/
c
c .... specify timestep for printout
c      data dtpr0,dtpr1,dtpr2,dtpr3,dtpr4,dtpr5,dtpr6/
c      1      .001,.001,.001,.001,.001,.001,.001/
c
c ...rubber flap dimensions and constants
c      a=.054
c      b=.0151
c      tv=.00635
c      er=540000.
c      cdamp=2.6
c      freq=4.35
c      ro=a-b
c      dv=2.*a
c      dvi=2.*b
c ...dimensions of hydram
c      h=1.89
c      dp=0.053
c      tp=.0032
c      al=9.85
c      alram=.40
c      alo=.0125
c      do=.0045
c      dor=.0517
c      de=8.*.0254
c      ddv=.0311
c      ymax=.0096
c      gapmax=.012
c ... property constants and pressure
c      den=1000.
c      vis=.00116
c      pi=3.1416
c      ew=2.17e9
c      es=1.90e11
c      pois=.3
c      poisr=.4
c      ef=1./ew+(5.-4.*pois)*.25*dp/(tp*es)
c      ef=1./ef
c      papsi=14.7
c      pa=101325.
c .... pdgpsi is the delivery pressure (psig)
c      pdgpsi=21.
c      pd=pa*(pdgpsi+papsi)/papsi
c      pdg=pd-pa
c      pstat=den*9.81*h
c
c ccccccccccccccc pressure loss coefficients ccccccccccccccc
c
c      cp=3.5
c      ce=0.
c      cd=1.3
c      ca=1.3
c      cr1=1.
c      cr2=-1.
c      co=1.
c      cdv=.3
c ... other weighting constants

```

```

fadv=.2
eff=1.
fydot=.75
fdt=1.
pcr=1.
cr=cr1
cop=co
c aaaaaaaaaaaaaaaaaaaaaa compute areas and area ratios aaaaaaaaaaaaaaaaaaaaaa
pid4=.25*pi
ao=pid4*dor*dor
aa=pid4*(de*de-dv*dv)
av=pid4*(dv*dv-dvi*dvi)
ap=pid4*dp*dp
ae=pid4*de*de
arm=ymax*pi*dv
adv=pid4*ddv*ddv
aroa=ao/aa
arorm=ao/arm
arop=ao/ap
arpo=ap/ao
arva=av/aa
aroe=ao/ae
ardvp=adv/ap
c ***** calculate area-corrected pressure coefficients *****
cte=aroe*aroe*ce
ctp=arop*arop*cp
ctd=aroa*aroa*cd
cta=aroa*aroa*ca
ctda=ctd+cta
ctr=arorm*arorm*cr
ct=ctd+cta+ctr
c oooooooooooooooooooooo oscillation parameters oooooooooooooooooooooo
vmass=av*tv*den
det=den*9.81*(a**4-b**4)*(1.-poisr*poisr)
wn=freq*sqrt(er*tv*tv/det)
cdampt=cdamp*0.5*den*av
c
c bbbbbbbbbbbbbbbbbbbbbbb start of each cycle bbbbbbbbbbbbbbbbbbbbbbb
nc=0
cmax=9.81*den*h
tilim=100.
tstart=0.
xi=0.
xim1=0.
yc=0.
c
10 vpi=1.0e-20
voi=1.0e-20
vp4=0.
npe=0
qiv=0.
qdv=0.
qwaste=0.
vpim1=0.
vomax=0.
vpmax=0.
vpt=0.000001
yim1=0.
yi=0.
t1=tstart
t2=tstart
ti=tstart
dt=dt1
dtpr=dtpr1
np=1
akti=1.

```



```

      vol=0.  
      yv=yi+xi  
      yvm1=yim1+xim1  
  
C     tttttttttttt   start of time step within each cycle   tttttttttttttttt  
C  
      do 730 i=2,nmax  
        dt0=dt  
        if(dtpr0.ne.100.)dtpr=dtpr0  
        ns=dtpr/dt  
        go to (100,200,300,400,500,600),np  
C ***** compute velocity in drive pipe *****  
C  
C    1111111111111111111111111111 period one 1111111111111111111111111111  
C  
100 co=0.  
    ctda=0.  
    ctd=0.  
    ctr=0.  
    tim1=ti  
    ti=ti+dt  
    vol=vol+ap*vpi*dt  
    yvol=vol/ae  
    if(yvol.ge.yc)go to 110  
    vpim1=vpi  
    call vpipe  
    if(vpi.gt.vpmax)vpmax=vpi  
    call oscil(xi,xim1,dt0,dt,xip1)  
    yi=xip1  
    xim1=xi  
    xi=xip1  
    if(float(i-2)/float(ns).ne.float((i-2)/ns))go to 105  
    if(nwrite.eq.1)write(3,30)i,ti,yi,vpi,pr,qtot,np  
105 continue  
    go to 730  
110 write(*,*)'PERIOD ONE PASSED'  
    np=3  
    dt=dt3  
    dtpr=dtpr3  
    t1=ti  
    go to 730  
  
C  
C    2222222222222222222222222222 period two 2222222222222222222222222222  
C  
200 co=cop  
    ctd=aroa*aroa*cd  
    cta=aroa*aroa*ca  
    ctda=ctd+cta  
    ctr=arorm*arorm*cr  
    tim1=ti  
    ti=ti+dt  
    if(vpi.ge.vpt)go to 210  
    vpim1=vpi  
    call vpipe  
    if(vpi.gt.vpmax)vpmax=vpi  
    qwaste=qwaste+ap*vpi*dt  
    go to 700  
210 write(*,*)'PERIOD TWO PASSED'  
    np=3  
    dt=dt3  
    dtpr=dtpr3  
    t2=ti-t1  
    go to 730  
  
C  
C    3333333333333333333333333333 period three 3333333333333333333333333333  
C
```

```

300 co=cop
    iydot=0
    tim1=ti
    ti=ti+dt
    if(ti.gt.tilim)dt=fdt*dt3
    yip0=1.
    vpim1=vpi
c
310 gap=ymax-yi
    if(gap.lt.0.)gap=0.00000001
    if(gap.gt.gapmax)gap=gapmax
    cr=cr1+cr2*(gap/gapmax)**pcr
    ctd=aroa*aroa*cd
    cta=aroa*aroa*ca
    ctda=ctd+cta
    ar=pi*dv*gap
c
    arvo=av/ao
    aror=ao/ar
    ctr=aror*aror*cr
    ydot=(yi-yim1)/dt
c
    teta=asin(yi/ro)
    rocos=ro*cos(teta)
    dvol=pi*ro*ro*ydot*(a/rocos+.66667)
c
    var=aroa*voi-ydot-dvol/aa
    rvadvo=var/voi
    ctda=ctda*rvadvo*rvadvo
    if(var.lt.0.)ctda=-ctda
c
    vr=aror*voi-dvol/ar
    rvrdvo=vr/voi
    ctr=cr*rvrdvo*rvrdvo
    if(vr.lt.0.)ctr=-ctr
c
    call vpipe
c
    ct=ctda+ctr
    p35=.5*den*voi*voi*ct
    if(p35.gt.cmax)p35=cmax
c
    call ydist(p35,yip1)
c
    if(yip1.lt.ymax)go to 320
    write(*,*)'PERIOD THREE PASSED'
    yi=ymax
    xi=0.
    xim1=0.
    voi=0.
    vpi=0.
    vomax=0.
c
    write(3,30)i,ti,yi,vpi,pr,vomax,np
c
    write(3,48)
    np=4
    tilim=.8*ti
    t3=ti-t2-t1
    sq=0.
    ac=sqrt(ef/den)
    pe=2.*al/ac
    hvpi=0.
    t40=ti
    np44=100
    dt=dt4
    dtpr=dtpr4
    dpmaxg=vpmax*sqrt(den*ef)

```



```

if(prt.lt.pdg)go to 420
tadv=tadv+dt
fradv=tadv/qpe
pmpd=2.*(prt-pdg)/den
vp4=fadv*fradv*cdv*adv*sqrt(pmpd)/ap
dq=ap*vp4*dt
dsq=dsqt+dq
sq=dsq
dqtot=qtot-dsq
pmt=pmtm1-(pmtm1-pdg)*dsq/qtot
slope=(pmt-prtm1)/(tqpe+dt)
itn=itn+1
if(itn.le.5)go to 410
go to 430
420 vp4=0.
430 continue
if(float(k-2)/float(ns).ne.float((k-2)/ns))go to 440
if(nwrite.eq.1)write (3,30)k,ti,yi,vp4,prt,dqtot,np41
440 continue
450 dt=dt4
np41=42
c write (3,30)k,ti,yi,vp4,pmrt,dqtot,np41
460 continue
tim1=ti
ti=ti+dt
c
anpe1=t400+float(npe)*pe
anpe2=anpe1+.5*pe
if(ti.ge.anpe1.and.ti.lt.anpe2)go to 480
npe=npe+1
to=ti
tm=ti+.5*pe
c
do 470 in=1,50
ti=ti+dt
if(ti.ge.tm)go to 475
if(float(in-2)/float(ns).ne.float((in-2)/ns))go to 470
if(nwrite.eq.1)write (3,30)in,ti,yi,hvpi,pr,qtot,np
470 continue
475 ti=tm
go to 485
480 continue
c
pr=pmt-(pmt-pdg)*sq/qtot+1.e-20
if(pr.le.pdg)go to 485
pmpd=2.*(pr-pdg)/den
vp4=cdv*adv*sqrt(pmpd)/ap
dq=ap*vp4*dt
sq=sq+dq
vpi=vp4
hvpi=.5*vpi
qdv=qdv+ap*vpi*dt
485 continue
if(float(i-2)/float(ns).ne.float((i-2)/ns))go to 490
if(nwrite.eq.1)write(3,30)i,ti,yi,hvpi,pr,qtot,np
490 continue
qstop=qtot-1.e-10
if(sq.lt.qstop)go to 730
write(*,*)'PERIOD FOUR PASSED'
np=5
dt=dt5
dtpr=dtpr5
dt50=2.*al/ac
t50=ti
t60=ti+dt50
t4=ti-t3-t2-t1

```

```
G
C 55555555555555555555555555555555 period five 55555555555555555555555555555555
C
500 tral=2./((den*ap*al)
    rerg=serg+werg
    vp5=-sqrt(rerg*tral)
    p50=pdg
    p60=pstat-.5*den*vp5*vp5
C
    xi=ymax
    xim1=ymax
C
    do 510 it=1,2000
        tim1=ti
        ti=ti+dt
        vpi=(ti-t50)*vp5/dt50
        voi=vpi*arpo
C
        pr=p50-(ti-t50)*(p50-p60)/dt50
C
        call oscil(xi,xim1,dt0,dt,xip1)
        yi=xip1
        xim1=xi
        xi=xip1
C
        if(ti.ge.t60)go to 520
        if(float(it-2)/float(ns).ne.float((it-2)/ns))go to 510
        if(nwrite.eq.1)write(3,30)it,ti,yi,vpi,pr,qtot,np
510 continue
C
520 vpi=vp5
    vp6=vp5
    kt5=1.+cp+ce
    pr=pstat-.5*den*vpi*vpi
    pr6=pr
C      write(3,30)i,ti,dt,vpi,pr,vomax,np
C      write(3,50)
    write(*,*)'PERIOD FIVE PASSED'
    np=6
    dt=dt6
    dtpr=dtpr6
    t5=ti-t4-t3-t2-t1
    t60=ti
    yc=0.
    go to 730
C
C 66666666666666666666666666666666 period six 66666666666666666666666666666666
C
600 tim1=ti
    ti=ti+dt
    tg=ti-t50
    vpin=-vpi
    re=den*vpin*dp/vis
    if(re.gt.2100)go to 610
    f=64./re
    go to 620
610 f=.316/(re**.25)
620 continue
    akt=1.+ctp+cte+f*al/dp
    bb=-9.81*h/al-.5*vpin*vpin*akt/al
    vipn=bb*dt+vpin
    vpin=vpin
    vpi=-vpin
    voi=vpi*arpo
    pr=pstat-.5*den*vpi*vpi
```

```

yc=yc+vpin*dt*ap/ae
call oscil(xi,xim1,dt0,dt,xip1)
yi=xip1
xim1=xi
xi=xip1

C
if(vpi.ge.0.)go to 640
if(float(i-2)/float(ns).ne.float((i-2)/ns))go to 630
if(nwrite.eq.1)write(3,30)i,ti,yi,vpi,pr,yc,np
630 continue
go to 730
640 nc=nc+1
write(*,*)'PERIOD SIX PASSED'
t6=ti-t5-t4-t3-t2-t1
beat=60./(ti-tstart)
if(nc.ge.ncycle)go to 740
tstart=ti
go to 10

C
C ooooooooooooooooooooooo output control oooooooooooooooooooooooooooooo
C
700 if(i.ne.2)go to 710
C write (3,47)
C write (3,40)cp,cdv,cd,ca,cr,cop,pdgpsi
C write (3,46)
710 if(float(i-2)/float(ns).ne.float((i-2)/ns))go to 730
if(nwrite.eq.1)write (3,30)i,ti,yi,vpi,pr,var,np
730 continue
740 continue
write(3,54)
write(3,52)t1,t2,t3,t4,t5,t6,beat
write(3,51)
qwcycle=qwaste*1000.
qtcycle=qtot*1000.
write (3,30)i,ti,yc,vpmax,pr,pmaxg,np
qwlpm=qwaste*beat*1000.
qtlpm=qtot*beat*1000.
write (3,53)
write (3,52)akemax,werg,serg,qwcycle,qtcycle,qwlpm,qtlpm
write (3,43)qwlpm
write (3,44)qtlpm
write (3,45)beat
close(3)
30 format(i5,5x,5(1pe10.3),i5)
40 format(6f10.3,1pe10.3)
52 format(7(1pe10.3))
43 format(/34h THE WASTE WATER FLOWRATE IS ,f10.3,27h
1LITRES PER MINUTE)
44 format( /34h THE DELIVERY WATER FLOWRATE IS ,f10.3,27h
1LITRES PER MINUTE)
45 format( /34h THE NUMBER OF BEATS IS ,f10.3,27h
1 BEATS PER MINUTE)
46 format(/64h i t(i) y(i) vp(i) pr v
1omax np)
48 format(/65h i t(i) sq vp(i) pr
1qtot np)
49 format(/65h i t(i) period vp(i) pr v
1omax np)
50 format(/65h i t(i) yc vp(i) pr v
1omax np)
51 format(/65h i t(i) yc vpmax pr pm
1axg np)
47 format(/67h cp cdv cd ca cr
1co pdgpsi)
53 format(/67h akemax werg serg qwcycle qtcycle qw
1lpm qtlpm)

```

[illegible]

```
      if(reo.gt.2100.)go to 1030
      fo=64./reo
      go to 1040
1030  fo=.316/(reo** .25)
1040  continue
```

C

```
      akt=1.+co+ctp+cte+ctda+ctr+arop*arop*f*al/dp
1      +fo*alo/do
      bb=.5*voi*voi*akt/al
      vpi=(9.81*h/al-bb)*dt+vpim1
      voi=vpi*arpo
      pr=pstat-.5*den*vpi*vpi
      return
      end
```

C
